

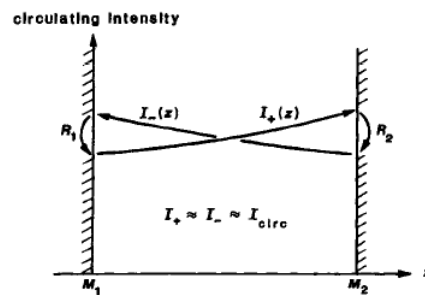
# LASER OUTPUT POWER

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## *Lightly Coupled Laser Oscillator*

A laser oscillator in which the reflectivities of the laser end mirrors are not too much less than unity.



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## Intensity Growth

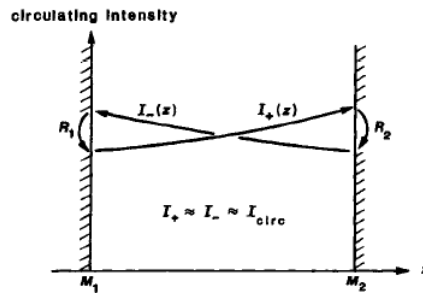
The growth of two oppositely traveling waves  $I_+(z)$  and  $I_-(z)$  inside the cavity:

$$\frac{dI_+(z)}{dz} = [2\alpha_m(z) - 2\alpha_0] I_+(z)$$

$$\frac{dI_-(z)}{dz} = -[2\alpha_m(z) - 2\alpha_0] I_-(z)$$

Saturated gain coefficient:

$$2\alpha_m(z) = \frac{2\alpha_{m0}}{1 + [I_+(z) + I_-(z)] / I_{\text{sat}}}$$



*The interference between the right- and left-traveling waves is neglected.*

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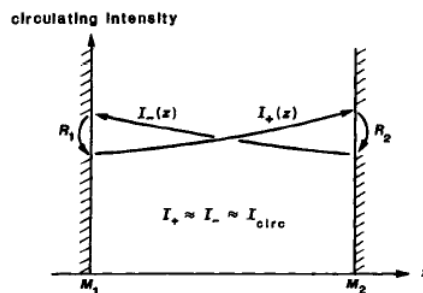
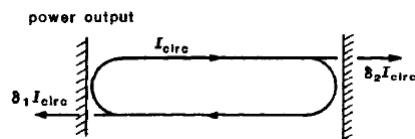
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## Small Output Coupling

$$R_1 = R_2 \approx 1$$

$$I_+(z) \approx I_-(z) \approx I_{\text{circ}}$$

$$2\alpha_m \approx \frac{2\alpha_{m0}}{1 + 2I_{\text{circ}} / I_{\text{sat}}}$$



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## *Steady-State Oscillation*

**Condition:**

$$2\alpha_m P_m \approx \frac{2\alpha_{m0} P_m}{1 + 2I_{\text{circ}}/I_{\text{sat}}} = 2\alpha_0 P + \ln\left(\frac{1}{R_1 R_2}\right) = \delta_0 + \delta_1 + \delta_2$$

The circulating intensity that must build up in order to saturate the gain down to where it just equals the total cavity losses:

$$I_{\text{circ}} = \left[ \frac{2\alpha_{m0} P_m}{\delta_0 + \delta_1 + \delta_2} - 1 \right] \times \frac{I_{\text{sat}}}{2}$$

$$I_{\text{circ}} = [r - 1] \times \frac{I_{\text{sat}}}{2}$$

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## *Power Output*

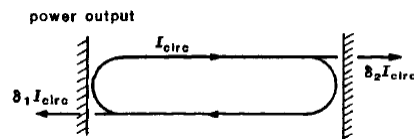
For a lightly coupled laser cavity:

$$T_1 = 1 - R_1 \approx \delta_1, T_2 = 1 - R_2 \approx \delta_2$$

$$I_{\text{out}} = (\delta_1 + \delta_2) \times I_{\text{circ}} = \delta_e \times I_{\text{circ}}$$

$\delta_e$ : External cavity coupling

$$I_{\text{out}} = \delta_e \left[ \frac{2\alpha_{m0} P_m}{\delta_0 + \delta_e} - 1 \right] \times \frac{I_{\text{sat}}}{2}$$



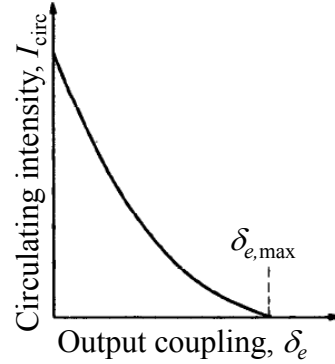
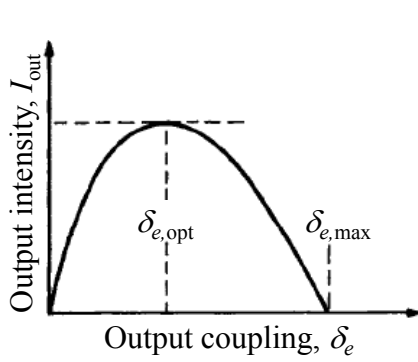
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## Output Coupling

$$I_{\text{out}} = \delta_e \left[ \frac{2\alpha_{m0} P_m}{\delta_0 + \delta_e} - 1 \right] \times \frac{I_{\text{sat}}}{2}$$

$$I_{\text{circ}} = \left[ \frac{2\alpha_{m0} P_m}{\delta_0 + \delta_e} - 1 \right] \times \frac{I_{\text{sat}}}{2}$$



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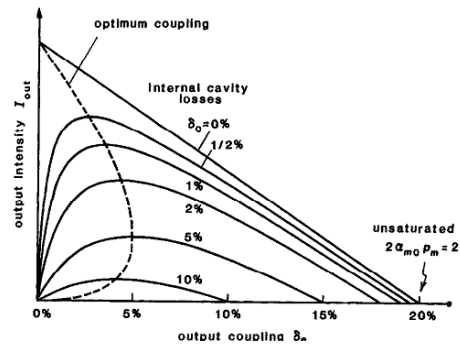
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## Optimum Output

$$\frac{dI_{\text{out}}}{d\delta_e} = \frac{d}{d\delta_e} \left\{ \delta_e \left[ \frac{2\alpha_{m0} P_m}{\delta_0 + \delta_e} - 1 \right] \times \frac{I_{\text{sat}}}{2} \right\} = 0$$

$$\delta_{e,\text{opt}} = \sqrt{2\alpha_{m0} P_m \delta_0} - \delta_0$$

$$I_{\text{out,opt}} = \left[ \sqrt{2\alpha_{m0} P_m} - \sqrt{\delta_0} \right]^2 \times \frac{I_{\text{sat}}}{2}$$



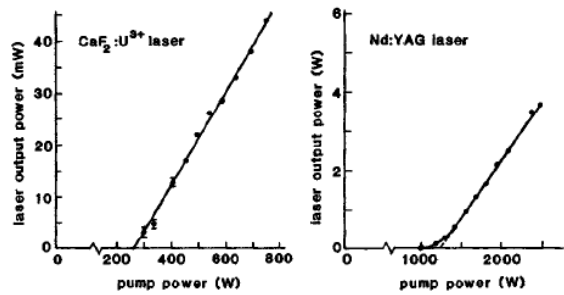
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## Power Output Vs. Pumping

$$r = \frac{2\alpha_{m0}P_m}{\delta_0 + \delta_e} = \frac{R_p}{R_{p,th}} = \frac{\text{pumping power}}{\text{threshold pump power}}$$

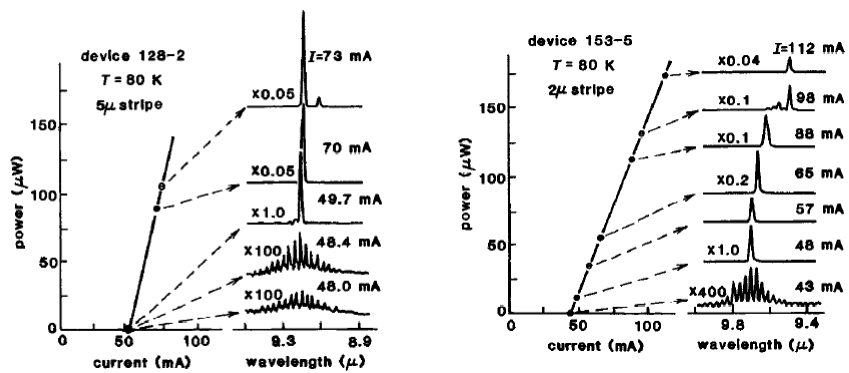
$$I_{out} = \frac{(r-1)\delta_e I_{sat}}{2} = \left[ \frac{R_p}{R_{p,th}} - 1 \right] \times \frac{\delta_e I_{sat}}{2}$$



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## Power Output & Output Spectra

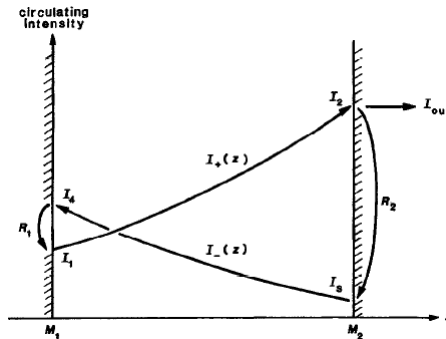


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## Large Output Coupling

- An analysis with arbitrarily large round-trip gain and output coupling was developed by W. W. Rigrod, and is often referred to as the “Rigrod Analysis.”
- Large output coupling.



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## Intensity Growth

Assume no distributed loss, i.e.,  $2\alpha_0 p = 0$ .

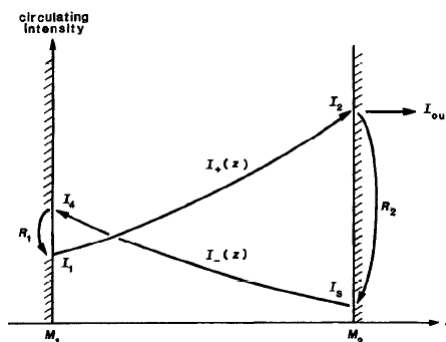
$$\frac{dI_+(z)}{dz} = +2\alpha_m(z)I_+(z)$$

$$\frac{dI_-(z)}{dz} = -2\alpha_m(z)I_-(z)$$

Let us assume that  $I_+(z)$  and  $I_-(z)$  are normalized to the saturation intensity  $I_{\text{sat}}$ .

$$\alpha_m(z) = \frac{\alpha_{m0}}{1 + I_+(z) + I_-(z)}$$

**The interference between the right- and left-traveling waves is neglected.**



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## *Intensity Growth*

$$I_-(z) \frac{dI_+(z)}{dz} = +2\alpha_m(z)I_+(z)I_-(z)$$

$$I_+(z) \frac{dI_-(z)}{dz} = -2\alpha_m(z)I_-(z)I_+(z)$$

$$\frac{d}{dz}[I_+(z)I_-(z)] = -2\alpha_m I_+ I_- + 2\alpha_m I_+ I_- = 0$$

$$I_+(z)I_-(z) = \text{constant} = C$$

$$\frac{dI_+(z)}{dz} = \frac{2\alpha_{m0}I_+(z)}{1 + I_+(z) + C/I_+(z)}$$

Integrating:  $\int_{I_1}^{I_2} \left(1 + \frac{1}{I_+} + \frac{C}{I_+^2}\right) dI_+ = 2\alpha_{m0} \int_0^L dz$

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## *Intensity Growth*

**For  $I_+(z)$ :**  $2\alpha_{m0}L = \ln\left(\frac{I_2}{I_1}\right) + I_2 - I_1 - C\left(\frac{1}{I_2} - \frac{1}{I_1}\right)$

**For  $I_-(z)$ :**  $2\alpha_{m0}L = \ln\left(\frac{I_4}{I_2}\right) + I_4 - I_3 - C\left(\frac{1}{I_4} - \frac{1}{I_3}\right)$

Mirror power reflectivities:

$$I_1 = R_1 I_4, \quad I_3 = R_2 I_2$$

$$I_2 = \frac{1}{(1+r_2/r_1)(1-r_1r_2)} \left[ 2\alpha_{m0}L - \ln\left(\frac{1}{r_1r_2}\right) \right]$$

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## Power Output

$$I_2 = \frac{1}{(1+r_2/r_1)(1-r_1r_2)} \left[ 2\alpha_{m0}L - \ln\left(\frac{1}{r_1r_2}\right) \right]$$

$$I_{\text{out}} = T_2 I_2 = \frac{T_2 I_{\text{sat}}}{(1+r_2/r_1)(1-r_1r_2)} \left[ \ln G_0 - \ln\left(\frac{1}{r_1r_2}\right) \right]$$

Maximum intensity that can be extracted:

$$I_{\text{avail}} = 2\alpha_{m0}L_m I_{\text{sat}} = (\ln G_0) I_{\text{sat}}$$

Power extraction efficiency:

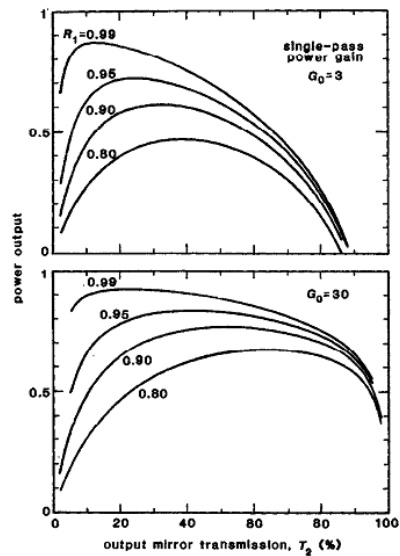
$$\eta = \frac{I_{\text{out}}}{I_{\text{avail}}} = \frac{T_2}{(1+r_2/r_1)(1-r_1r_2)} \left[ 1 + \frac{\ln r_1r_2}{\ln G_0} \right]$$

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## Power Output

- $\eta$  is not much less than 1 for large  $G_0$  and  $R_1$ .
- Output coupling level in a high-gain laser is not a critical factor.
- $R_1 \rightarrow 100\%$  and  $T_2 \leq 50\%$  for high output power.



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